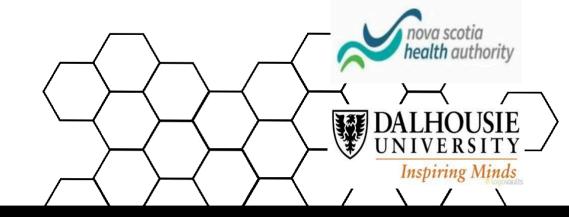


Algorithm for optimization of the x-ray beam and filter parameters in dual-energy imaging systems

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INTRODUCTION

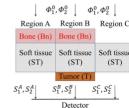
Dual-energy (DE) x-ray imaging has a long history of practical applications [1,2]. It requires acquiring two x-ray images with different spectra. Such spectra can be generated by changing x-ray tube voltage (kVp) and current (mAs). However, this is not enough to provide optimal conditions for high-quality DE acquisition. The conventional method is to introduce filtration of the x-ray beam through materials of varying thickness L and atomic number Z. Various combinations of filter Z and L, and tube kVp and mAsresult in DE images with different subject contrast and noise. In this study we propose an algorithm, which determines the optimal xray beam and filtration parameters, leading to the maximized quality of DE images, evaluated through the contrast-to-noise ratio.

This study aims to find optimal filtration for low- and high-energy beams (Z and L) and optimal x-ray tube parameters (kVp and mAs), which provide the maximum contrast-to-noise ratio (CNR), which was chosen as the figure of merit.

The optimization should include clinically related constraints, such as patient size, patient dose, detector dynamic range, and x-ray tube limits. Three patient sizes were considered: small, medium, and large [3]. For each size, the specific dose constraint was used. The dynamic range of ExacTrac (Brainlab AG, Germany) detector

METHOD

· A virtual phantom was used (Fig. 1) with geometry similar to the one used in experiments.



igure 1. Virtual phantom to calculate CNR. $\,\Phi^0_{1,2}$ are initial spectra of HE, LE beams with $S^{A,B,C}_{1,2}$ are the esulting signals of the attenuated spectra as incident at the detector for regions A, B, and C respectively

- Monte Carlo model [4] was used to obtain scatter-to-primary ratios (SPR) for different regions of interest.
- The analytical expression connecting DE CNR with input spectra and SPR was derived.
- Input x-ray spectra for each combination of kVp, mAs, Z, and L were simulated with customized Spektr3.0 software [4].
- Each combination of filter/beam parameters was checked against constraints on the flat panel detector dynamic range, patient sizes, and dose limitations. Constraints were taken from
- Obtained beam/filter parameters were manually unified, in order to reduce the variations in the choice of filters and their thicknesses, while retaining CNR near the optimal value.
- · Partial experimental verification was performed.

ALGORITHM

$$CNR = \frac{\frac{S_{1}^{A}}{(S_{2}^{A})^{\omega}} - \frac{S_{1}^{B}}{(S_{2}^{B})^{\omega}}}{\sqrt{\left(\frac{S_{1}^{A}}{(S_{2}^{A})^{\omega}}\right)^{2} \left[\left(\frac{\sigma_{1}^{A}}{S_{1}^{A}}\right)^{2} + \omega^{2}\left(\frac{\sigma_{1}^{A}}{S_{1}^{A}}\right)^{2}\right] + \left(\frac{S_{1}^{B}}{(S_{2}^{B})^{\omega}}\right)^{2} \left[\left(\frac{\sigma_{1}^{B}}{S_{1}^{B}}\right)^{2} + \omega^{2}\left(\frac{\sigma_{1}^{B}}{S_{1}^{B}}\right)^{2}\right]}}.$$

$$S_i = (1 + SPR) \int_0^{E_i^{-m}} \Phi_i(E) e^{-\sum \mu_i^k(E) t_k} E dE \sim f(Z, L, mAs),$$

and noise σ_i is

$$\sigma_i^2 = (1 + SPR) \int_0^{E_i^{max}} \Phi_i(E) e^{-\sum \mu_i^k(E) t_k} E^2 dE \sim f(Z, L, mAs).$$

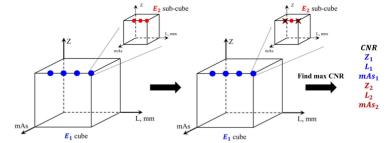
Calculations were performed for a combination of low and high energy (E_1^{max} and E_2^{max}) beams from 60 to 140 kVp with 10 kVp increments. Current, filter material and thickness were varied independently for low and high energies. Tube current varied from 1 to 90 mAs (ExacTrac limits), Filter thickness L varied from 0 to 2.0 mm with 0.2 mm increments. Filter materials were selected from the periodic table, with Z from 1 to 83, except for radioactive, gases, liquids, and highly reactive elements. For one energy pair these parameters form a 6D space. At each point, three quantities were calculated: CNR, equivalent surface dose (ESD), and air kerma at the detector surface

$$CNR \sim f(Z_1, L_1, mAs_1, Z_2, L_2, mAs_2),$$

 $ESD \sim f(Z_1, L_1, mAs_1, Z_2, L_2, mAs_2),$
 $Air\ kerma \sim f(Z_1, L_1, mAs_1, Z_2, L_2, mAs_2).$

ESD was calculated as per AAPM TG-61 protocol, and the dose constraint was such that the DE dose is less than clinically established single energy dose. Detector dynamic range is expressed in terms of air kerma at the detector surface. The resulting data was represented as nested cubes, where each cube is

After the constraints were applied (Fig. 2) the maximum CNR value was found, and the corresponding combination of parameters was obtained. The same procedure was repeated for each combination of kVp and the overall maximum was determined. The same procedure was repeated over all patient sizes.



gure 2. Algorithm flow and data representation. On the left, there is a "cube" in Z_1, L_1, mAs_1 coordinates. Each point is a -cube" in Z_2, L_2, mAs_2 . Each point in this "sub-cube" is the CNR, Dose or Air kerma va

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RESULTS

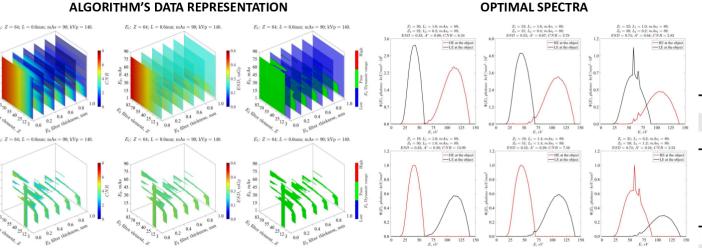


Figure 3. Top row: 3D "cube" of CNR, ESD, and dynamic range ($Air\ kerma$) for one set of Z_1, L_1, mAs_1 parameters om row CNR, ESD, and dynamic range (Air kerma) with applied system constrain for bone only images. From left to right: high, medium, and large patient sizes

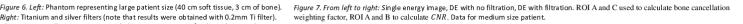
ADJUSTED NEAR OPTIMAL PARAMATERS

| | Beam | | | | | Fil | ter | A * | CNR | |
|--------|-------|-------|-------|-------|-------|-------|-------|------------|------|------|
| Size | kVp | | mAs | | Z | | L | | | |
| | E_1 | E_2 | E_1 | E_2 | E_1 | E_2 | E_1 | E_2 | | |
| Small | 140 | 60 | 75 | 80 | 47 | 22 | 1.0 | 0.2 | 0.32 | 6.13 |
| Medium | 140 | 70 | 90 | 90 | 47 | 22 | 1.0 | 0.2 | 0.68 | 4.81 |
| Large | 140 | 90 | 90 | 90 | 47 | 22 | 1.0 | 0.2 | 0.77 | 2.69 |
| | | | | | | | | | | |

| | Beam | | | | | Fil | ter | A * | | |
|--------|-------|-------|-------|-------|-------|-------|-------|------------|------|-------|
| Size | kVp | | mAs | | Z | | L | | CNR | |
| | E_1 | E_2 | E_1 | E_2 | E_1 | E_2 | E_1 | E_2 | | |
| Small | 60 | 140 | 80 | 70 | 22 | 47 | 0.2 | 1.0 | 0.4 | 19.46 |
| Medium | 70 | 140 | 90 | 90 | 22 | 47 | 0.2 | 1.0 | 0.32 | 11.80 |
| Large | 80 | 140 | 90 | 90 | 22 | 47 | 0.2 | 1.0 | 0.23 | 4.81 |

Table 3.4: DE parameters for soft tissue (top) and bone (bottom) only images with no filtration

EXPERIMENTAL RESULTS PHANTOM AND FILTERS $CNR_{DE} = 2.98$ (w filter). $CNR_{DE} = 2.07$ (w/o filter).



| | | | Ве | am | | | | |
|------|--------|-------|----------------|-------|-------|------------|-------|--|
| Size | | kl | ['] p | m. | As | A * | CNR | |
| | | E_1 | E_2 | E_1 | E_2 | | | |
| | Small | 140 | 60 | 4 | 62 | 0.61 | 2.89 | |
| | Medium | 140 | 70 | 7 | 57 | 0.57 | 1.96 | |
| | Large | 140 | 90 | 6 | 51 | 0.74 | 1.29 | |
| | | | Be | am | | | | |
| | Size | kl | 'p | m. | As | A^* | CNR | |
| | | E_1 | E_2 | E_1 | E_2 | | | |
| | Small | 60 | 140 | 62 | 4 | 0.39 | 14.30 | |
| | Medium | 60 | 140 | 90 | 7 | 0.43 | 9.17 | |
| | Large | 80 | 140 | 63 | 8 | 0.34 | 3.25 | |
| | | | | | | | | |

DISCUSSION AND CONCLUSIONS

Filters were installed on a 3D printed holder, to compensate for the oblique angle.

The developed algorithm allows for optimization of the filtration and beam parameters, leading to maximized CNR, while considering all clinical constraints, such as patient dose, detector dynamic range, and x-ray tube operational ranges. The core of the algorithm is the expression, which relates input spectra to the output DE image CNR. This model has several simplifications. First, scatter contribution was included by using the scatter-to-primary ratio, without considering the energy shift between primary and scattered photons. Second, the detector is assumed ideal, and the noise was estimated without considering the detector's quantum efficiency, energy absorption, read-out noise, or scatter contributions. Full experimental verification is undergoing (delayed due to COVID-19); nonetheless, the preliminary experimental results showed that materials identified by the algorithm indeed increase the image CNR.

The algorithm is implemented in Matlab and determines the optimal set of parameters by computing over 10^9 possible combinations. In order to optimize execution time, the Matlab parallelization toolbox was used. The average run time for one patient size for one type of image (bone or soft-tissue) was reduced to about 1.5 hours. The total optimization time (all patient sizes, bone, and soft tissue images) is about 9 hours.

Optimization was conducted for ExacTrac system parameters, but the algorithm, in general, can be implemented for any system. The optimal filtration pair was identified for each patient's size. This resulted in a combination of three pairs of filters with different materials and thicknesses. This set was reduced to a combination of two materials with different thicknesses, namely:

⁴⁷Ag, 1.0mm for HE and ²²Ti, 0.2mm for LE.

Corresponding optimal beam parameters can be found in Tables 1,2.

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